

PASSIVE COOLING OF ELECTRONIC COMPONENTS USING CLOSED ALUMINIUM HOUSING FILLED WITH LIQUID

Janis Galins, Aigars Laizans, Ainars Galins

Latvia University of Life Sciences and Technologies, Latvia

janis.galins@llu.lv, aigars.laizans@llu.lv, ainars.galins@llu.lv

Abstract. The use of digital data transmission equipment has increased rapidly in recent years. There is a need for more powerful, more compact equipment that can deliver the required data transfer intensity. More powerful processors and radio signal transmission circuits require more power, and the energy losses are emitted as increasing heat flux, bringing in substantial risks of equipment overheating, thus reducing the device's reliability and causing overall faults of the devices. Aggressive environmental conditions are common in the bioeconomy product processing industries, and the devices used often suffer from inappropriate design of cooling solutions, including both active and passive systems. The electronic devices require airtight design, which protects from extensive moisture and corrosive gases. Passive cooling solutions are more reliable and do not consume any energy, but they have less heat transfer capacity than active cooling. Efficient solution could be passive cooling with convection, if the inside of the unit's body is filled with dielectric fluid such as oil. The study carries out heat transfer and fluid flow simulations in the electronic device to show how the heat flow dissipates in the environment using passive cooling design. Convection and conduction efficiency is analysed to find a way to implement a technical solution for new product development. As a result of the study, it has been found that the closed housing heatsink does not protect the component from overheating, if the air inside the housing is a heat transfer fluid. The use of heat bridges or filling the inside of the casing with a dielectric heat transfer fluid was more efficient. The studies have shown that semiconductors can be effectively cooled using liquid heat transfer fluids, such as ester MIDEI 7131.

Keywords: cooling system, heat modelling, heat transfer, heat convection.

Introduction

The housing of majority of electrical equipment has air inside, making it easier to repair and replace the damaged electronic elements, but heat transfer through the convection is not effective enough. The industrially used airtight housing design sometimes includes filling the casing with polyurethane, but the polyurethane acts as a thermal insulation and the convection inside is reduced. Passive cooling solutions are more reliable and do not consume any energy, but they have less heat transfer capacity than active cooling. Efficient solution could be passive cooling with convection, if the inside of the unit's body is filled with a dielectric fluid. Different types of insulating fluids are used for cooling applications. Heat from the hot components is dissipated in the environment by convection. This technology is already used for cooling high power transformers. Research studies indicate that the cooling capacity of the alternative liquid worsens with aging due to the exponential decrease of the viscosity with temperature [1]. Synthetic ester ages considerably slower than the natural ester dielectric fluid and mineral oil under the same aging conditions [2]. Heat transfer efficiency is greatly influenced by the thermal conductivity, specific thermal conductivity, viscosity and the expansion coefficient of the heat transfer fluid.

As the liquid heats up, the viscosity decreases, thereby increasing the fluid flow rate and cooling efficiency [3-5]. Other research studies show that the maximum temperatures of natural ester – filled transformers are only several degrees higher than those in mineral oil – filled transformers [6-8]. The thermal properties of insulating fluids are shown in Table 1.

The higher viscosity of the natural ester fluid is partly compensated by better thermal conductivity. Synthetic ester MIDEI 7131 is a widespread and tested dielectric coolant. It is designed to provide an alternative to mineral oil, silicone liquid and dry-type transformers. The main benefits of MIDEI 7131 are described below. The high fire point of 316 °C significantly increases the fire safety and reduces the need for fire protection equipment. Ester MIDEI 7131 is biodegradable in nature, thus reducing the risk of contamination if leakage occurs. MIDEI 7131 can be an effective solution in colder climates due to low pour point of -56 °C. Perfectly suited for non-free-breathing and free-breathing applications due to its excellent stability of oxidation [1; 2].

Table 1
Thermal properties of insulating fluids [6;9]

Property	Mineral oil	Natural esters	Synthetic esters
Thermal conductivity at 20 °C, W·(m·K) ⁻¹	0.126	0.160-0.167	0.144
Specific heat in 20 °C, J·(kg·K) ⁻¹	1860	1883-1943	1880
Thermal expansion coefficient, °C ⁻¹	0.00075	0.00068-0.00074	0.00075
Kinematic viscosity at 0 °C, mm ² ·s ⁻¹	37.5	207-276	240
Kinematic viscosity at 20 °C, mm ² ·s ⁻¹	22	78-97	70
Kinematic viscosity at 40 °C, mm ² ·s ⁻¹	9	36-42	28
Kinematic viscosity at 100 °C, mm ² ·s ⁻¹	2.6	8-9	8
Density in 20 °C, kg·m ⁻³	880	910-920	970

Materials and methods

The study uses a hermetic electrical device that is intended to be placed under aggressive environmental conditions. Inside the enclosure a semiconductor is placed on the PCB and emits a certain amount of heat. Passive cooling is used, because the fan is not allowed. Computational fluid dynamics (CFD) and heat transfer simulations were performed in Solidworks software. Only conduction and convection without radiation were used for heat transfer. The structure of the simulation model is shown in Fig. 1.

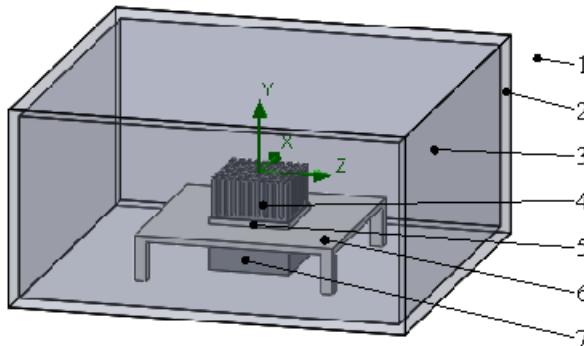


Fig. 1. Structure of simulation model: 1 – ambient air; 2 – enclosure; 3 – internal fluid; 4 – heatsink; 5 – semiconductor; 6 – printed circuit board; 7 – heat bridge

The ambient air with the temperature of 293.2 K is around the enclosure. Passive cooling solutions with heatsinks, heat bridges and liquid cooling with synthetic esterMIDEL 7131 have been tested to determine the most efficient. The solutions were compared both with dynamic changes in the temperature and with increasing the amount of heat generation from 1 to 10W. There was a need to create a new digital fluid for simulations using the thermal properties of synthetic esterMIDEL 7131, as shown in Table 2.

Table 2
Thermal properties of synthetic esterMIDEL 7131 over temperature range [6]

Temp- erature, °C	Temp- erature, °K	Kinematic viscosity, mm ² ·s ⁻¹	Specific heat, J·(kg·K) ⁻¹	Density, kg·m ⁻³	Thermal conductivity, W·(m·K) ⁻¹	Coeff. of thermal expansion, 1·K ⁻¹
-30	243.15	4200	1783	1007	0.145	0.00072
-20	253.15	1400	1797	1000	0.145	0.00073
-10	263.15	430	1811	992	0.145	0.00074
0	273.15	240	1830	985	0.145	0.00074
10	283.15	125	1855	978	0.145	0.00075
20	293.15	70	1880	970	0.144	0.00075
30	303.15	43	1910	963	0.144	0.00076
40	313.15	28	1933	956	0.143	0.00077
50	323.15	19.5	1959	948	0.142	0.00077

Table 2 (continued)

Temp-erature, °C	Temp-erature, °K	Kinematic viscosity, mm ² ·s ⁻¹	Specific heat, J·(kg·K) ⁻¹	Density, kg·m ⁻³	Thermal conductivity, W·(m·K) ⁻¹	Coeff. of thermal expansion, 1·K ⁻¹
60	333.15	14	1994	941	0.141	0.00078
70	343.15	10.5	2006	934	0.140	0.00078
80	353.15	8	2023	926	0.139	0.00079
90	363.15	6.5	2040	919	0.137	0.00079
100	373.15	5.25	2058	912	0.136	0.0008

Dynamic viscosity, specific heat, density, thermal conductivity vary depending on the temperature, so the graphs are used in the simulations. Solidworks flow simulations require dynamic viscosity, so calculations were made:

$$\mu = \rho \cdot v, \quad (1)$$

where μ – dynamic viscosity, Pa·s;
 ρ – density, kg·m⁻³;
 v – kinematic viscosity, mm²·s⁻¹.

Kinematic viscosity also depends on the temperature, as shown in Table 2. After the calculation the obtained graph is shown in Fig. 2.

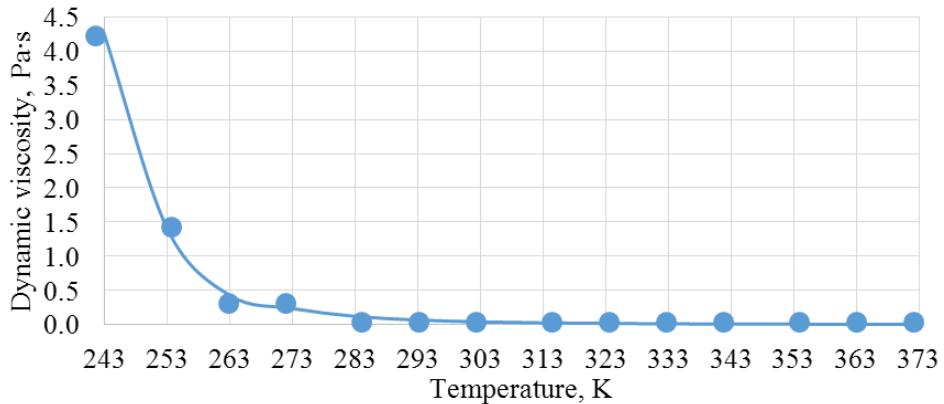


Fig. 2. DYNAMIC VISCOSITY OF ESTER MIDEI 7131 DEPENDING ON TEMPERATURE

Temperature fluctuations have a significant impact on the viscosity of the synthetic ester and the obtained graph is non-linear. The density graph and specific heat graph are linear, but the thermal conductivity does not change a lot depending on the temperature.

Input data were selected according to the model equipment and environmental conditions, as shown in Table 3.

Table 3
Input data for CFD and heat transfer simulations

Parameter	Value	Unit
Gravity in y axis direction	-9.81	m·s ⁻²
Atmospheric pressure	101325	Pa
Ambient temperature	293.2	K
Heat generation rate for semiconductor	1...10	W
Fluids type	Air; Ester MIDEI 7131	

The simulation results are significantly influenced by the selected solid materials, because each of them has a different thermal conductivity. The selected solid materials are shown in Table 4.

Table 4
Solid materials used for CFD and heat transfer simulations

Part	Size, mm	Material	Thermal conductivity, W·(m·K) ⁻¹ [10]
Semiconductor	20x20x1.5	Silicon	~150 (depends on temperature)
Printed circuit board (PCB)	50x50x1.6	Laminate FR4	0.3
Enclosure	100x100x50 (wall thickness 2mm)	Aluminium	~237 (depends on temperature)
Heatsink	20x20x10		
Heat bridge	20x20x10		

Results and discussion

Computational fluid dynamics (CFD) and heat transfer simulations were performed until the system reaches a steady-state. The research was done to state how the maximal temperature of the semiconductor depends on the heat generation rate. The results are shown in Fig. 3.

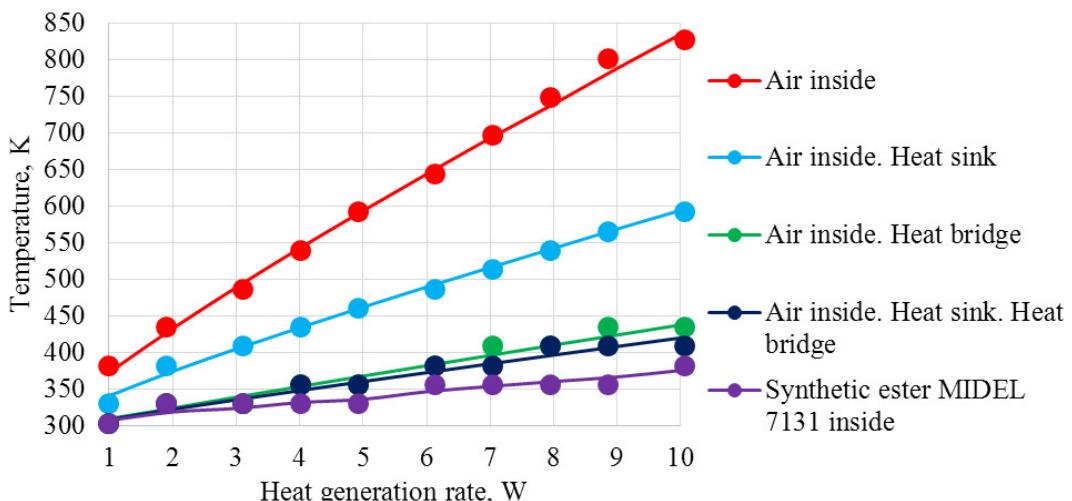


Fig. 3. Max temperature of semiconductor depending on heat generation rate

The “Air inside” curve represents the max temperature of the semiconductor depending on the heat generation rate, if no cooling solution is used. The “Air inside; Heat sink” represents a solution, when a heatsink is attached to the semiconductor and the internal fluid is air. Obviously, the most efficient solution is, when an internal fluid is esterMIDEL 7131. The obtained max temperature differences of the semiconductor were compared depending on the heat generation rate. Calculations have revealed how much the liquid cooling solution is better than the others, as shown in Table 5.

Semiconductor parts are most often specified for use in the “commercial” 0 to 70 °C (273.15 to 343.15 K) and in the “industrial” -40 to 85 °C (233.15 to 358.15 K) operating temperature range[11]. Manufacturers specify even higher safe operating temperatures. Graphics processing unit(GPU) such as Nvidia GTX 980 can exceed the maximum safe temperature of 98 °C (371.15 K), as specified in the specification of the manufacturer[12]. If the normal operating temperature of the semiconductor is 340 K, cooling with ester MIDEL 7131 is 48 % more efficient than cooling with the heatsink or 12 % more efficient than cooling with the heat bridge. Better heat transfer results could be obtained by using mineral oil due to its lower viscosity.

Dynamic CFD and heat transfer simulation of the semiconductor with heat generation 5 W was performed. The resulting heating curve of max temperature of the semiconductor shown in Fig. 4.

Most of electronic components must not exceed 120 °C (393.15K) operating temperatures. The graph shows that without cooling (“Air inside” curve) the maximum semiconductor temperature will exceed 393 K after 44 s and continues to increase damaging the semiconductor. The passive cooling solution with the heatsink only works for a short time, because after 57s it is more efficient to have a

heat bridge solution, but after 131 s the semiconductor temperature also will exceed 393 K. The solution with a heat bridge or liquid fluid can prevent overheating in this case. The best long time solution is cooling with ester MIDEL 7131. It surpasses cooling with a heatsink after 27 s.

Table 5
Comparison of different passive cooling solutions

Heat generation rate, W	Max temperature of semiconductor, if ester MIDEL 7131 is applied, K	Cooling with ester MIDEL 7131 is better than other solution, %		
		Air inside; Heat sink	Air inside; Heat bridge	Air inside; Heat sink; Heat bridge
1	306.9	51	4	2
2	318.4	49	5	3
3	323.3	49	9	7
4	331.3	48	10	8
5	335.8	48	12	9
6	346.2	48	12	9
7	353.5	48	12	9
8	360.1	48	13	10
9	366.3	48	14	10
10	375.2	48	14	10

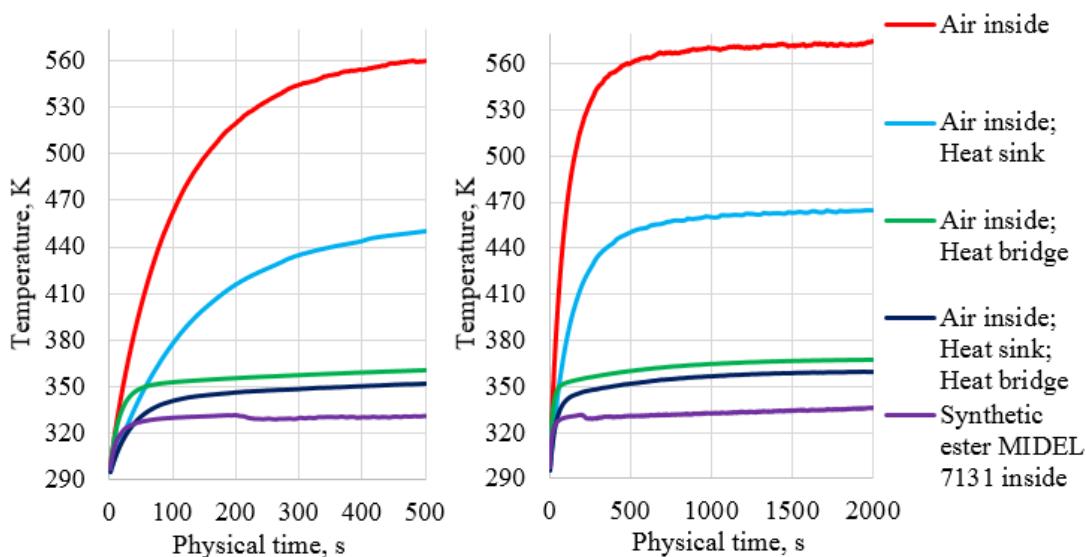


Fig. 4. Heating curve of max temperature of semiconductor with heat generation 5W

The dynamics of the heat transfer fluid was studied in time. Different distribution of the fluid temperature was observed after 50 s and 2000 s, as shown in Fig. 5.

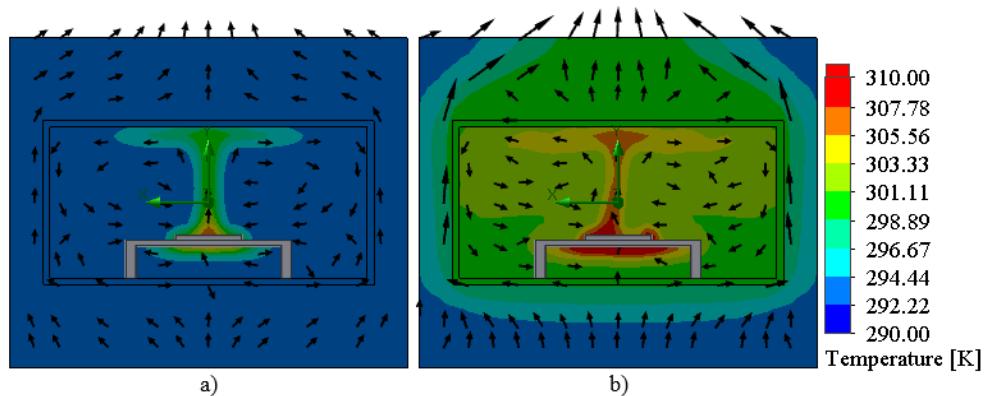


Fig. 5. Temperature of heat transfer fluid (ester MIDEL 7131 inside; air outside) in time with semiconductor heat generation 5 W: a – after 50 s; b – after 2000 s

The efficiency of the applied liquid heat transfer fluid depends on the working temperature. If the temperature rises, the viscosity decreases and the heat transfer improves. As the system stabilizes, the liquid fluid velocity decreases due to the decrease of the density difference. The temperature of the semiconductor in a particular enclosure reached its maximum 335.8 K after 2000 s with esterMIDEL 7131 applied.

Conclusions

1. Studies have shown that semiconductors can be effectively cooled using liquid heat transfer fluids, such as esterMIDEL 7131.
2. Cooling with ester MIDEL 7131 in a particular enclosure is 48 % more efficient than cooling with the heatsink or 12 % more efficient than cooling with the heat bridge.
3. The temperature of the semiconductor in a particular enclosure reached its maximum 335.8 K after 2000 s with esterMIDEL 7131 applied.
4. The efficiency of the applied liquid heat transfer fluid depends on the working temperature due to the viscosity, but as the system stabilizes, the liquid fluid velocity decreases due to the decrease of the density difference.
5. The passive cooling solution with the heatsink only works for a very short time, thus heat bridges or liquid cooling should be used for long time periods.

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